

[54] **SIDELOOKING LASER ALTIMETER FOR A FLIGHT SIMULATOR**

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[52] U.S. Cl. .... **356/1; 356/4; 358/104; 358/109; 434/4; 434/38**

[58] Field of Search ..... **434/4, 38; 356/1, 4; 358/109, 104**

[56] **References Cited**

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WO80/02455 11/1980 PCT Int'l Appl. .... 356/1

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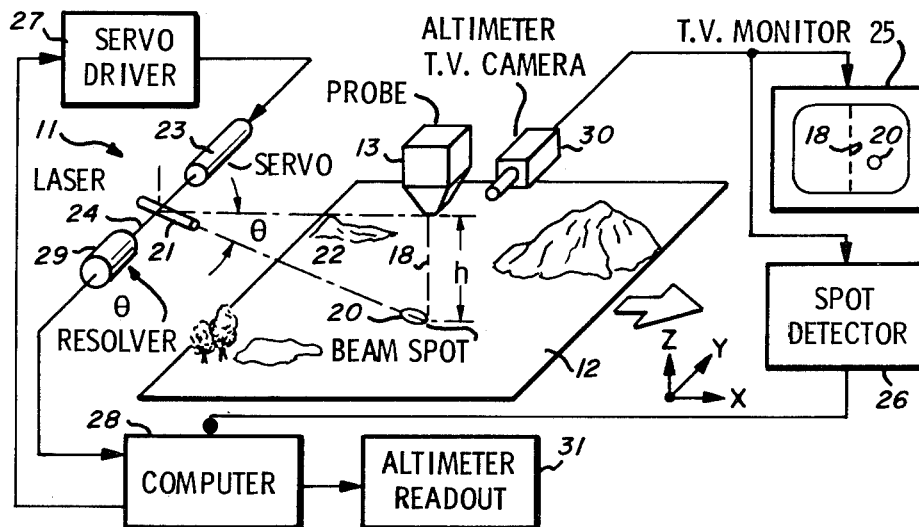
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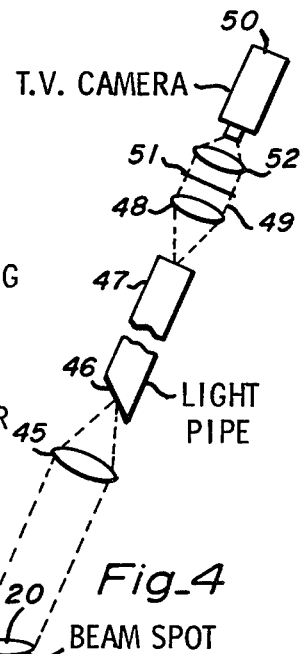
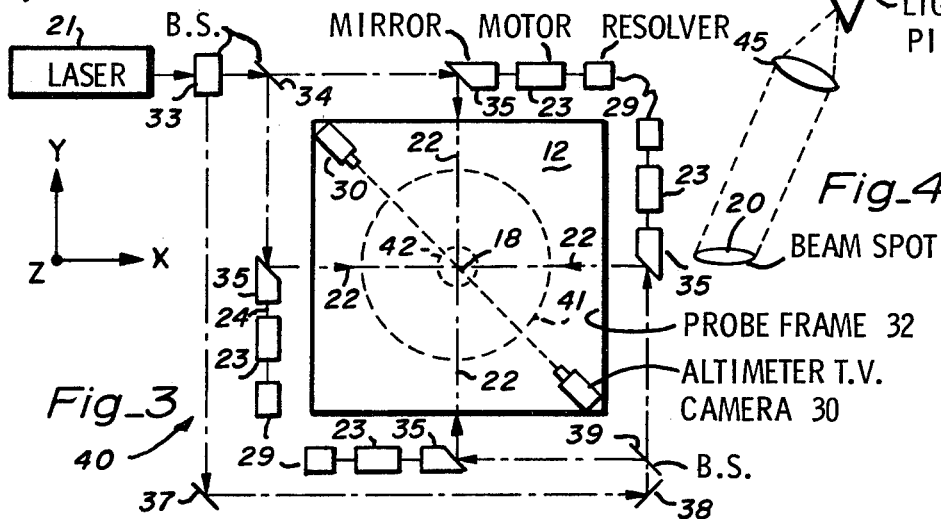
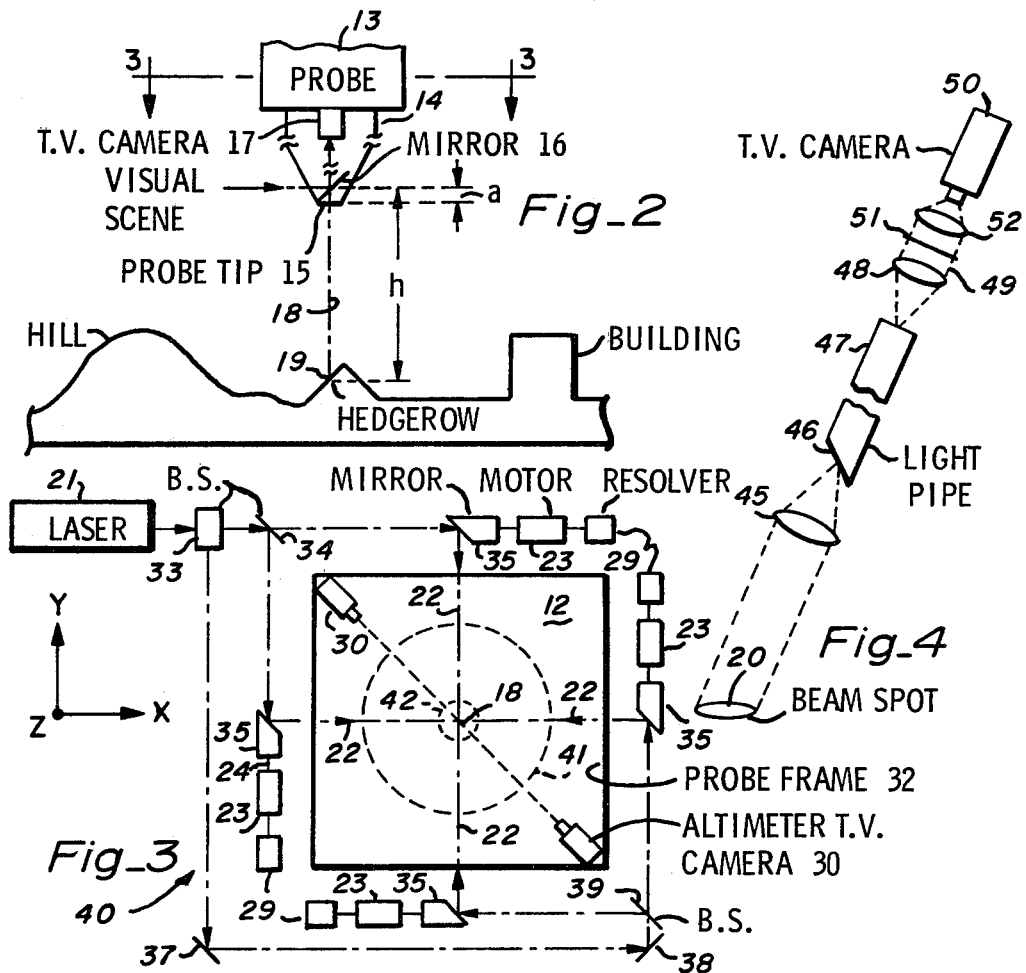
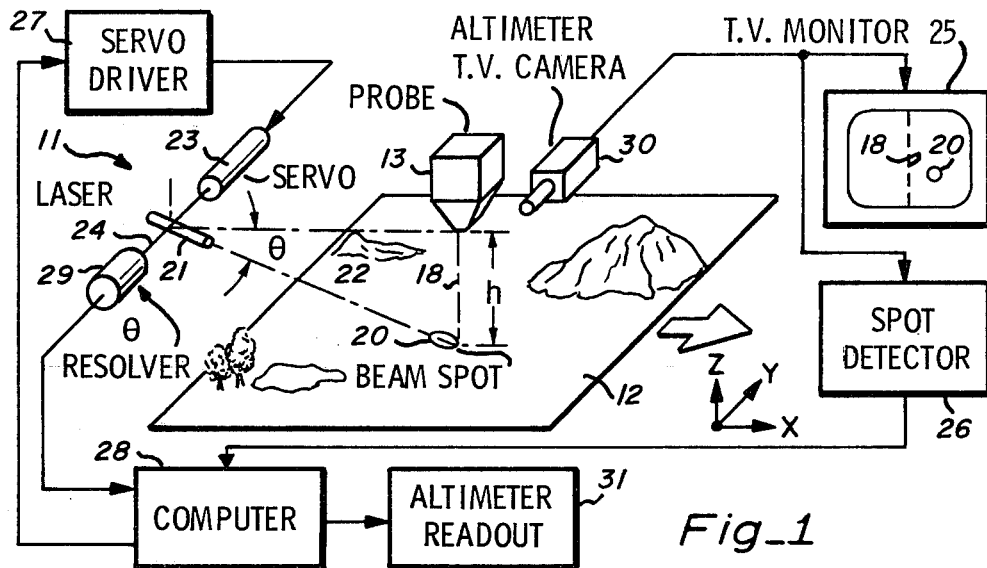
## ABSTRACT

The object of the invention is to provide an improved laser altimeter for a flight simulator which will allow measurement of the height of the simulator probe above the terrain directly below the probe tip.

A laser beam 22 is directed from the probe 13 at an angle  $\theta$  to the horizontal to produce a beam spot 20 on the terrain. The angle  $\theta$  that the laser beam 22 makes with the horizontal is varied so as to bring the beam spot into coincidence with a plumb line 18 coaxial with the longitudinal axis of the probe 13. A television altimeter camera 30 observes the beam spot and has a raster line aligned with the plumb line 18. Spot detector circuit 26 coupled to the output of the TV camera monitors the position of the beam spot relative to the plumb line 18. An error signal is produced by computer 28 driving, via a servo motor 23, the laser beam optics so as to cause the beam spot to come into coincidence with the plumb line 18. At coincidence, computer 28 looks up in a table the altitude of the probe for the given angle  $\theta$  and reads out the altitude to an altimeter readout 31.

**11 Claims, 9 Drawing Figures**





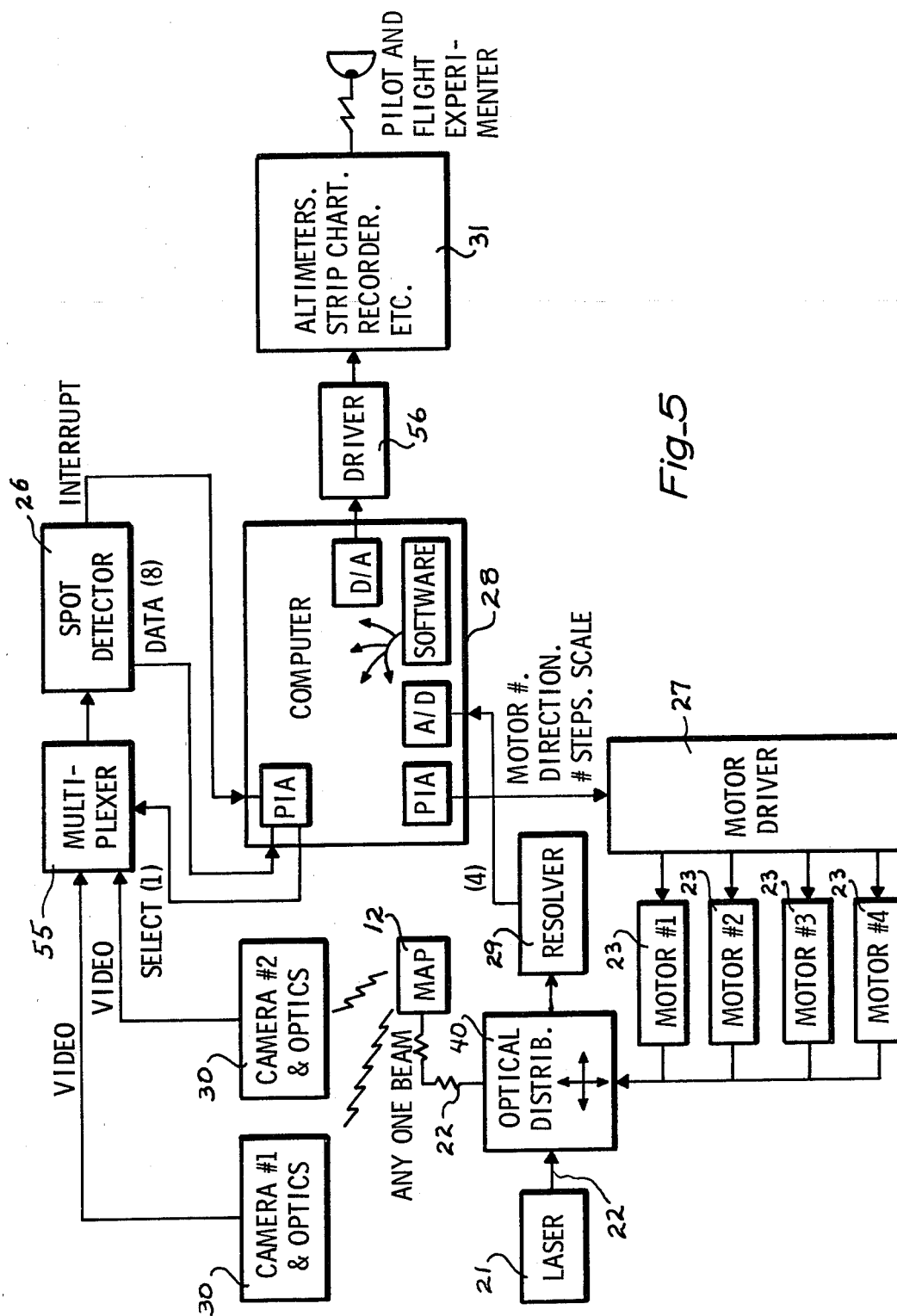
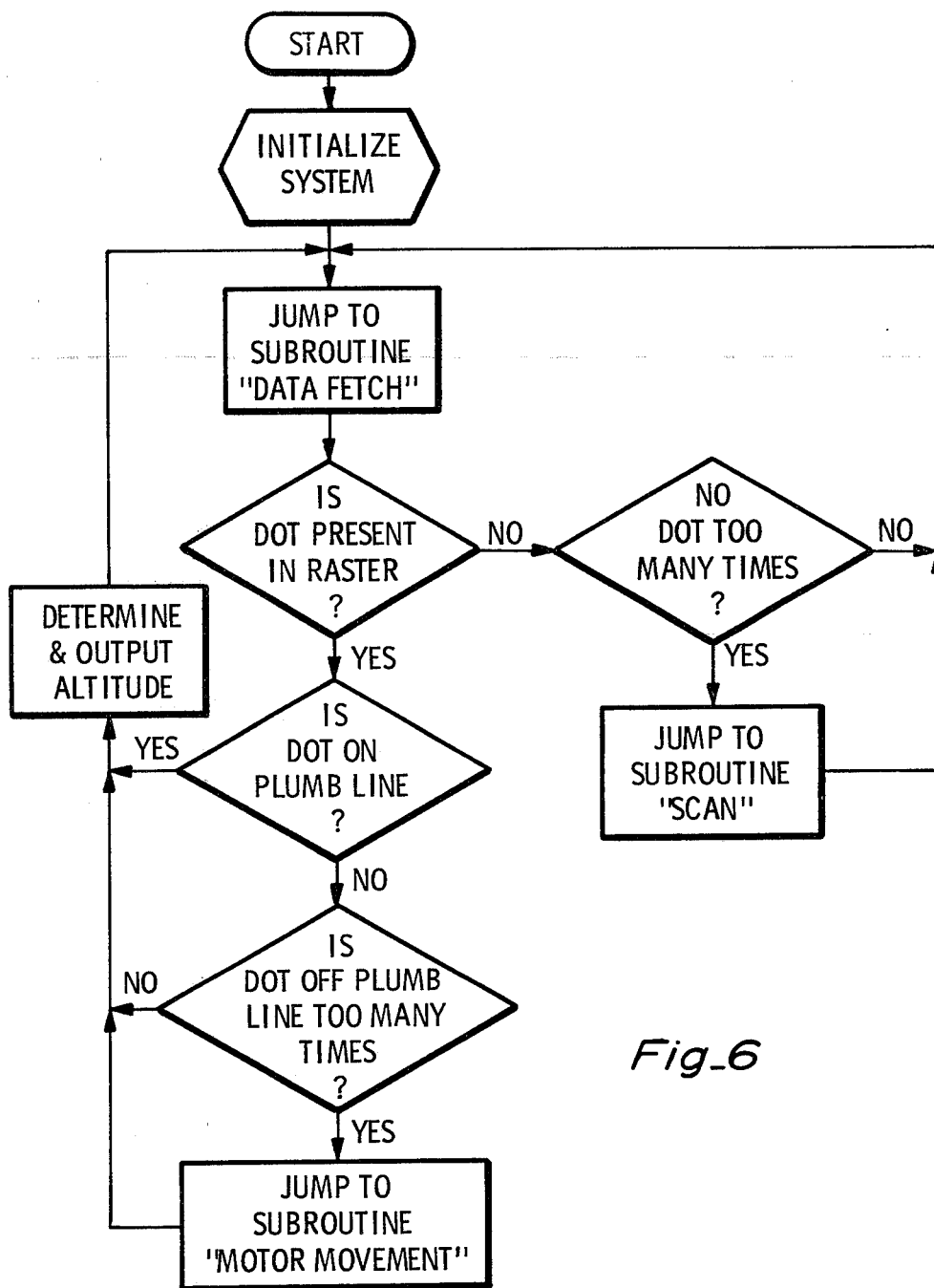
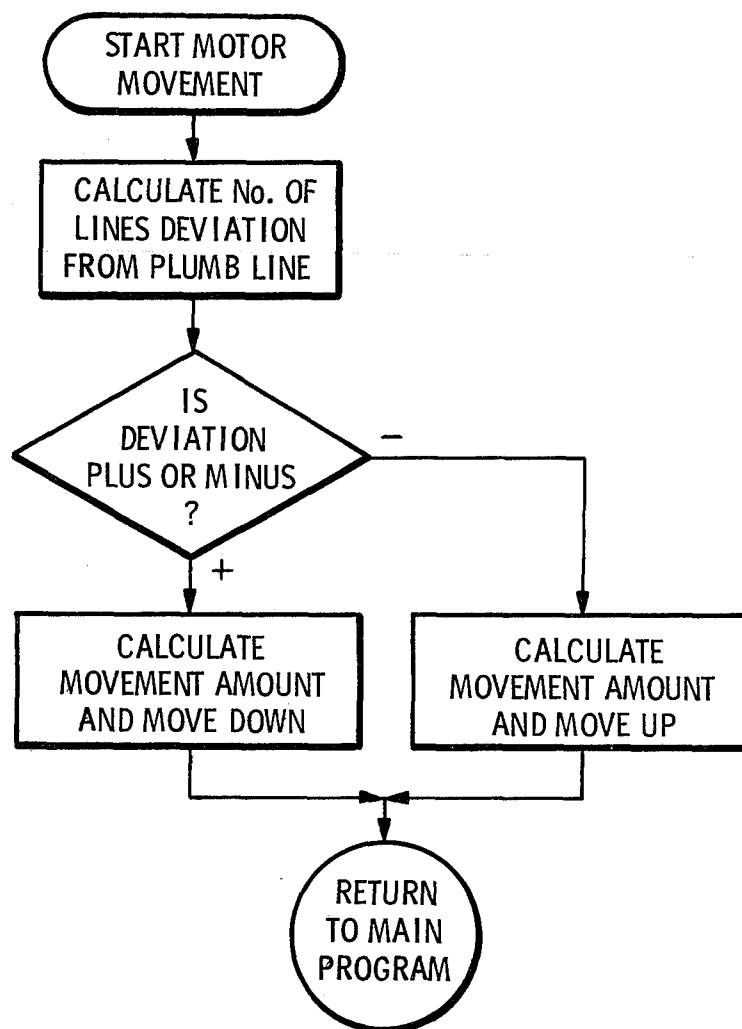
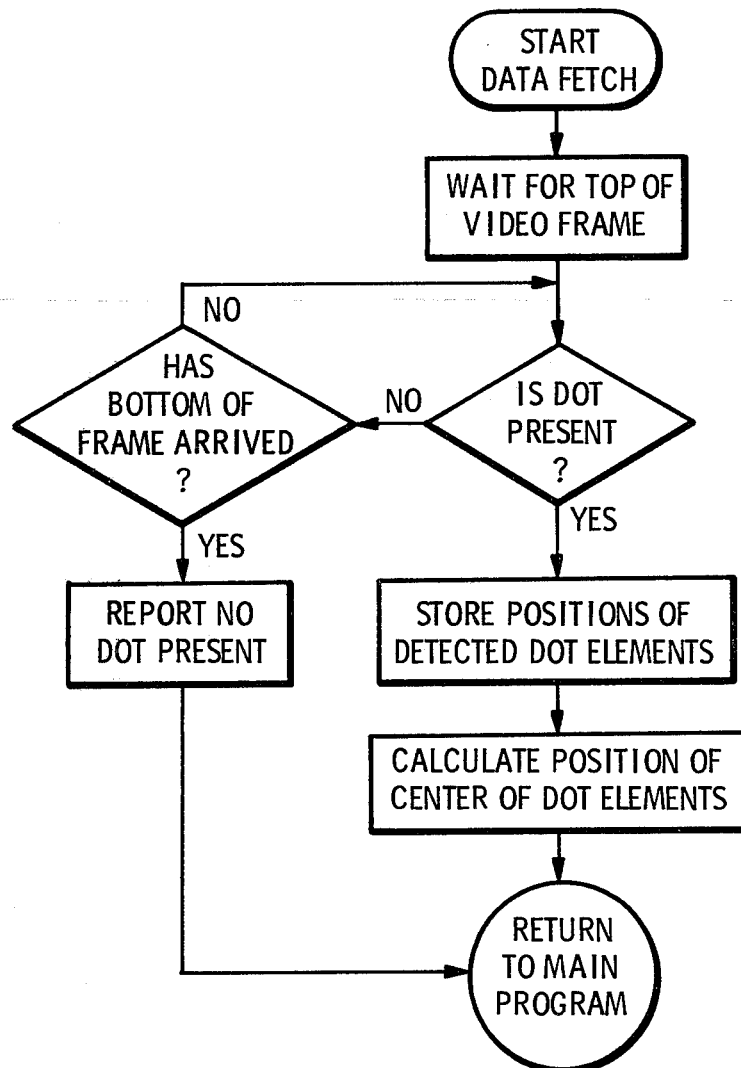
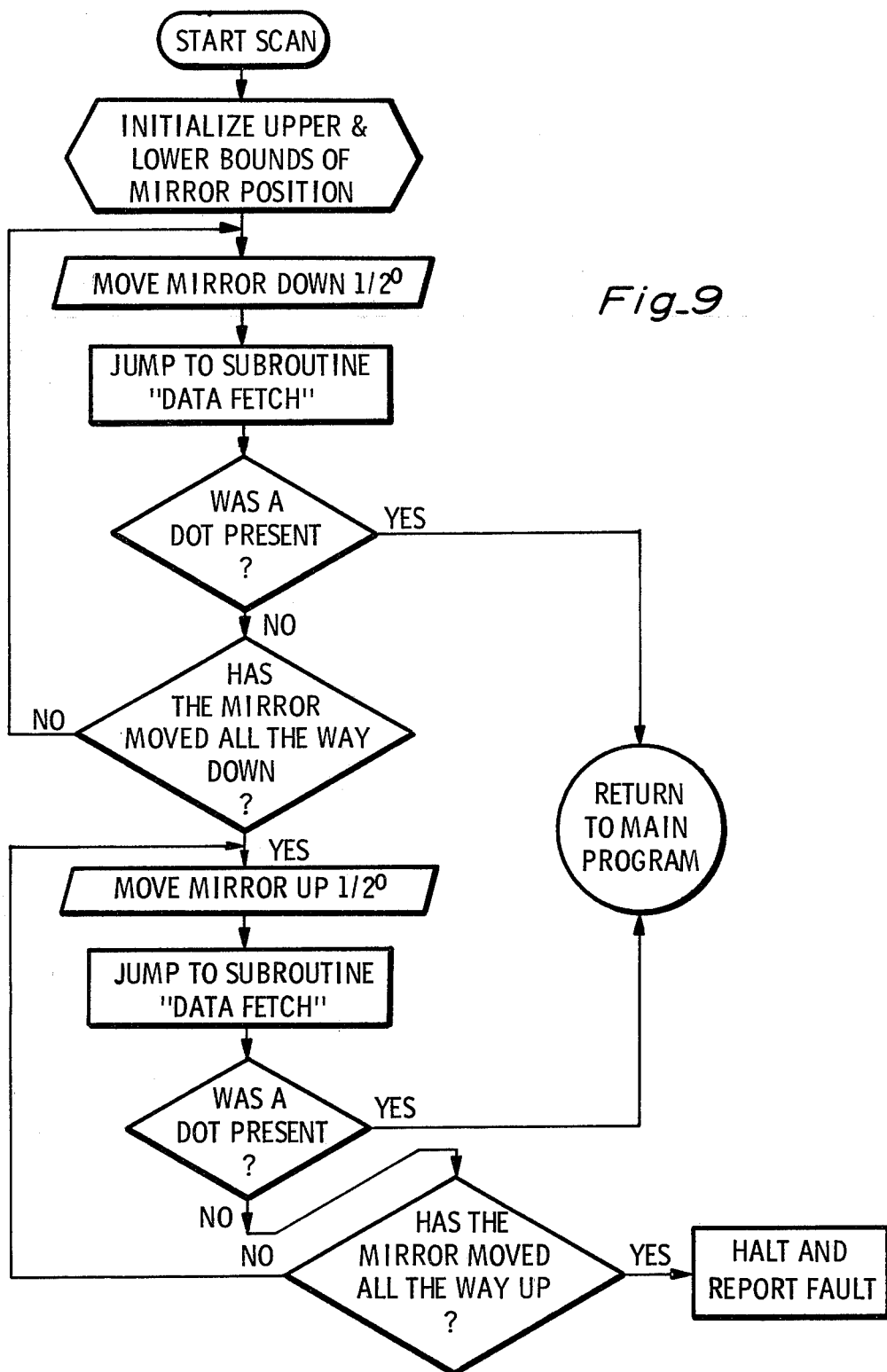


Fig. 5

*Fig-6*

*Fig-7*

*Fig. 8*



## SIDELOOKING LASER ALTIMETER FOR A FLIGHT SIMULATOR

### ORIGIN OF THE INVENTION

The invention described herein was made by an employee of the U.S. Government and may be manufactured and used by or for the Government for Governmental purposes without the payment of any royalties thereon or therefor.

### TECHNICAL FIELD

The technical field of the present invention relates in general to laser altimeters for flight simulators.

### BACKGROUND ART

Heretofore a laser altimeter system has been proposed for determining the altitude of a flight simulation probe over a model board. Such a prior art system is disclosed in an article entitled, "Probe Protection In Camera/Model Visual Systems" appearing in the Proceedings of the 1980 Summer Computer Simulation Conference, Olympic Hotel, Seattle, Wash., Aug. 25-27, 1980.

In this system, a laser beam is directed vertically from the flight simulator TV camera probe along a side of the probe to strike a point on the model board radially displaced from a point directly below the center line of the probe, hereafter referred to as a plumb line. The incident beam produces a beam spot on the terrain of the model which is thence imaged onto a linear array sensor. As the height of the probe is varied, while holding the probe otherwise stationary, from a point of minimum altitude to a point of maximum altitude the beam spot traverses a vertical imaginary line focused onto the linear array sensor. The position of the imaged beam spot along the linear array sensor is representative of altitude. A major problem with this system is that the altitude being measured is not the altitude of the probe (altitude measured along the plumb line) but rather the altitude of the laser beam source which is displaced horizontally from the probe. The actual distance between the plumb line and the laser beam must be multiplied by the scale of the model. Error will be produced whenever the terrain elevation at the plumb line differs from the terrain elevation at the laser beam. For example, an appreciable error would exist if the plumb line was over a depression and the laser beam impinged on a hill, mountain or tall building.

Thus, it is desirable to obtain a probe height sensor which more accurately measures the height of the probe above the terrain directly below the probe.

### [STATEMENT OF INVENTION]

### DISCLOSURE OF INVENTION

In the present invention, pilot altitude as represented by the distance  $h$  is measured by a technique that locates the point of intersection of the plumb line and the terrain (hereinafter known as the convergence point). A laser beam is directed from the probe at an angle to the plumb line and coaxial with the longitudinal axis of the probe. The point where the beam strikes the terrain is varied by changing the angle of the laser beam relative to the longitudinal axis of the probe so that the beam spot is brought to a point on the longitudinal axis of the probe where it intersects the terrain. A TV camera, carried from the probe views the region below the probe and has a predetermined linear detection region,

such as a raster line, coaxially aligned with the image of the plumb line. A detection circuit receives the output of the TV camera and determines the position of the laser dot in the raster. Using this information, a computer determines the position of the beam spot relative to the plumb line. A resolver coupled to the laser beam angle control reads out the angular position  $\theta$  of the laser beam to a computer. The computer looks up the height of the probe in a look up table for the angle  $\theta$  of the laser beam. The measured height is then read out to an altimeter and to a flight simulation monitor station. If the laser dot does not reside on the plumb line, a computer directs a stepper motor to relocate the beam such that the dot will reside on the plumb line. If the operative laser beam is unable to be relocated at the convergence point because it is blocked by a terrain obstruction, an alternative laser beam at a different angle around the probe is selected. Also, if the TV camera's view is blocked the computer selects an alternative TV camera.

### BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic perspective view, partly in block diagram form, of an altimeter system for a flight simulator incorporating features of the present invention,

FIG. 2 is a longitudinal sectional view of the flight simulator probe and model board,

FIG. 3 is a schematic transverse sectional view, partly in block diagram form, of a portion of the structure of FIG. 2 taken along line 3-3 in the direction of the arrows,

FIG. 4 is a schematic side elevational view of the TV camera optics for beam spot detection,

FIG. 5 is a schematic block diagram of a laser altimeter system incorporating features of the present invention,

FIG. 6 is a logic flow diagram for the computer program for the system of the present invention, and

FIGS. 7, 8, and 9 are logic flow diagrams for subroutines of the computer program flow diagram depicted in FIG. 6.

### DETAILED DESCRIPTION OF THE INVENTION

Referring now to FIG. 1 there is shown a laser altimeter system 11 for a flight simulator and incorporating features of the present invention. The flight simulator system includes a model board 12 comprising a scale model of terrain over which simulated flights are to be conducted. The pilot sits in a cockpit, not shown, and views a television screen displaying a view seen through a probe 13 movable with respect to the terrain of the model board 12 in accordance with flight control commands given by the pilot over the aircraft controls. The probe 13 is carried from a gantry, not shown, disposed over the terrain of the model board 12. Relative movement in three orthogonal directions, X, Y, and Z is obtained between the probe and the model board. In some embodiments, the gantry moves relative to a stationary model board to provide movement in all three orthogonal directions, whereas, in other embodiments the model board is moved relative to the probe to simulate flight.

Referring now to FIG. 2, the optical system for the probe 13 is shown in greater detail. More particularly, the probe 13 includes an elongated barrel portion 14



projecting in the Z direction toward the model board. At the end or tip of the probe 15 there is a mirror 16 which projects a visual scene corresponding to that which would be seen by the pilot, up along the longitudinal axis of the probe barrel 14 to a TV camera 17. The scene picked up by the TV camera is then transmitted to and displayed on a cathode ray tube outside the windshield of the simulated aircraft. The altitude  $h$  of the simulated aircraft is that scale distance from the mirror 16 is taken along a plumb line 18 for the modeled terrain to a point of intersection of the plumb line with the terrain at 19.

Referring again to FIG. 1, a laser 21 is carried from a frame coupled to and movable with the probe 13. The laser directs a pencil-like beam 22 of monochromatic nondivergent radiation of visible wavelength onto the terrain below the probe 13 having been deflected by pitchable mirror 35 to produce a beam spot 20 on the terrain. A servo motor 23 is coupled to the mirror 35 in such a way as to vary the angle  $\theta$  that the laser beam makes to the horizontal or XY plane of the model board 12. The laser beam is rotatable about an axis of revolution parallel to the horizontal XY plane and such beam being rotatable in a plane normal to said axis of revolution, such plane also containing the plumb line 18.

An altimeter TV camera optical system 30 is also carried from the probe frame. The altimeter TV camera system 30 includes some optics, not shown, and views the region of the model board directly below the probe 13. The TV camera optics are such that the point of intersection of plumb line 18 with the model board surface is within the view of the TV camera system 30 for all values of altitude  $h$  from minimum to maximum above the surface of the model board 12.

A single raster line is made coincident with the plumb line 18 through appropriate mechanical alignment. An output from the altimeter TV camera 30 goes to a spot detector circuit 26 of the type similar to that disclosed in U.S. Pat. No. 3,320,360 issued May 16, 1967 entitled, "Television Tracking Error Detector", for determination of the location of the beam spot 20 relative to the plumb line 18.

The output of spot detector 26 is fed to a computer 28. This output consists of the raster line number and displacement along the raster line of all of the detected elements of the laser spot 20. The computer determines the location of the center of the laser spot 20 in the raster of the altimeter TV camera system 30. To be coincident with the end of the plumb line 18, the laser spot 20 must lie somewhere along the altimeter TV camera system raster line which was made coincident with the plumb line 18. The computer 28 compares the raster line number of the center of the laser spot 20 with the raster line number of the raster line which is coincident with the plumb line 18. If the two are equal then the laser spot 20 must be located on the terrain at the end of plumb line 18 where it intersects the terrain. The exact length of plumb line 18 may then be determined. If the two are not equal, the laser spot 20 is not located at the end of plumb line 18 where it intersects the terrain. An error signal is generated which causes servo driver 27 to reposition laser spot 20 until the two raster line numbers are equal. The computer 28 also receives the angle  $\theta$  input from a resolver 29 mechanically coupled to the laser beam deflection system so that at the point of convergence of the beam spot 20 with the point of entry of the plumb line 18 into the terrain, the computer reads the  $\theta$  angle and looks up, in its look up table,

the value of altitude corresponding to the given values of altitude for various values of  $\theta$  as the probe is moved from a position of minimum altitude to maximum altitude over the model board.

Referring now to FIG. 3 there is shown the optical distribution system for deriving the various laser beams and for televising the beam spot 20 on the model board. The laser 21 is affixed to a probe frame member 32, and directs its output beam through first and second beam splitters 33 and 34. Beam splitter 33 is arranged to direct the reflected portion of the beam downward along the Z axis whereas the other half of the beam passes through the first beam splitter 33, to the second beam splitter 34 which serves to further divide the beam into a first beam directed parallel to the X axis and a second beam of equal amplitude directed along the Y axis. Each of the beams outputted from the second beam splitter 34 is directed onto a 45° angle mirror 35 for bending the respective beam by 90° toward the plumb line 18. Each of the mirrors is driven from a stepping servo motor 23 about respective axes of revolution. In one instance the axis of revolution is parallel to the X axis and in the other to the Y axis and both are in the XY plane so as to cause the beams to be rotated within respective planes which are perpendicular to the XY plane and each of which includes the plumb line 18. A  $\theta$  angle resolver 29 is coupled to each of the motor-mirror drive trains for giving an output determinative of the angle  $\theta$ .

The other half of the output of the first beam splitting mirror 33 is directed downward along the Z axis to a 45° mirror, not shown, which thence directs the beam parallel to the Y axis to a second 45° mirror 37 and thence parallel to the X axis to another 45° mirror 38 which thence directs the beam through a second beam splitting mirror 39 for splitting the beam into two equal components, one parallel to the Y axis and the other parallel to the X axis. The beams are then reflected off of respective 45° mirrors 35 driven from the stepping motors 23 which include resolvers 29. Thus, the second beam produces a pair of beams directed onto the model board 12 which are orthogonal to each other and which are 180° displaced from the first pair of beams. The beams are rotatable in the XZ and YZ planes, such planes each including the plumb line 18. The respective mirrors 35 are positioned such that their output beams will intersect the plumb line 18 at the point that the plumb line 18 intersects the surface of the model 12.

The orthogonality between each of the laser beams is not a requirement. For example, it could be three beams at 120° angular spacing from each other with the camera optics similarly angularly separated from each other by 120° and being spaced at 60° angles from each of the respective beams.

A pair of altimeter TV camera optics are carried from the probe frame structure 32 and are positioned at 180° intervals about an axis of revolution coaxial with the plumb line 18 and preferably at 45° angular spacing from the ZX or ZY planes but on the XY plane containing the respective laser beams. This positioning of the altimeter TV camera optics 30 permits viewing of the respective beam spot 20 at the plumb line 18, regardless of various buildings, hills, or trees or other obstructions in the terrain of the model board 12. In other words there is some combination of laser beam 22 and altimeter TV camera optics 30 which will permit viewing of the beam spot 20 at the plumb line 18 regardless of the obstructions represented by the terrain of the model 12, with the exception of a well or deep ravine. The laser

beams 22 which are not in use, i.e., three of the four are "parked" by rotating their respective mirrors 35 so as to project the beam spot 20 onto the probe body 41 or 42.

Referring now to FIG. 4 there is shown one of the optical systems 30 for each of the TV altimeter cameras. More particularly, a condensing lens 45 receives the light emanating from the beam spot 20 and focuses the image of the beam spot onto the entrance plane 46 of a light pipe 47 such as a fiber optics bundle. The bundle 47 may have a suitable length as of 3-5 feet to bring the image of the beam spot 20 to a convenient location of the TV camera 50, typically somewhere on the gantry. Another lens 48 receives the beam spot image at the output face of the light pipe 47 and converts the image into a beam of parallel light 49 which is thence directed through a narrow pass filter 51 having a pass band at the wavelength of the laser beam 22 so as to filter out undesired background illumination. The filtered beam is thence fed to a condensing lens 52 which focuses the beam spot image onto the receiving face of the TV camera 50. The input face of the light pipe 46 is cut at the Scheimpflug angle, as described in U.S. Pat. No. 751,347 issued Feb. 2, 1904, so that the plumb line 18 of the probe is maintained in focus on the input face of the TV camera 50.

Referring now to FIG. 5 there is shown, in block diagram form, the laser altimeter system 11 of the present invention. The output beam 22 of the laser 21 is fed through an optical distribution system 40 as shown in FIG. 3. One of the output beams 22 is selected and directed onto the terrain of the model 12 under the probe 14. The beam spot image 20 is picked up by both of the camera optical systems 30. Their output video signals are fed to a multiplexer 55. The computer 28 selects one or the other of the camera optic systems 30

and feeds a control signal to the multiplexer 55 for controlling which one of the camera optic systems 30 is utilized. The output of the multiplexer 55 is fed to the spot detector 26 which tracks the image of the beam spot 20 relative to the plumb line 18 which is inputted to the computer 28 and thence outputted to the motor driver 27 and respective motor 23. In a typical example, the computer 28 comprises a Motorola 6800 Exorcisor. The resolver 29 outputs the angle  $\theta$  for the selected beam 22 to an analog-to-digital converter in the computer 28. When the computer 28 detects zero error, i.e., the beam spot is at the plumb line 18, the computer 28 by its software looks up in a table the altitude corresponding to the respective angle  $\theta$  and outputs that data via a digital-to-analog converter to a driver 56 which thence inputs it to the altimeters or other read out devices 31.

Referring now to FIG. 6, there is shown the logic flow chart for the software program for the computer 28. FIGS. 7-9 depict the logic flow charts for program subroutines, namely, MOTOR MOVEMENT, DATA FETCH, and SCAN, respectively. The program listing is shown in Appendix I, below.

One of the advantages of the laser altimeter system of the present invention for a flight simulator includes detecting the altitude of the probe above a position directly below the probe as opposed to a position displaced in the horizontal plane from the probe. This makes the concept inherently accurate. Secondly, the provision of angularly displaced laser beams 22 and camera optics 30 allows reading of the altitude regardless of the obstructions represented by features in the terrain which might otherwise obstruct viewing of the beam spot.

## APPENDIX I

```

00010 00001
00020 00002
00030 00003
00040 00004
00050 00005
00060 00006
00070 00007A 5000
00080 00008
00090 00009A 5000 019F A CONV FDB $019F CONVERGENT RASTER LINE
00100 00010A 5002 04 A SHMV FCB $4 SMALL MVT THRESHOLD
00110 00011A 5003 08 A MDMV FCB $8 MEDIUM MVT THRESHOLD
00120 00012A 5004 10 A LGMV FCB $10 LARGE MVT THRESHOLD
00130 00013A 5005 03CF A BIAS FDB $03CF BIAS FOR ALTIM. ZERO
00140 00014A 5007 7F EF41 A CLR $EF41 SET UP COLECT PIA'S
00150 00015A 500A 7F EF43 A CLR $EF43
00160 00016A 500D 7F EF51 A CLR $EF51
00170 00017A 5010 7F EF53 A CLR $EF53
00180 00018A 5013 7F EF40 A CLR $EF40
00190 00019A 5016 7F EF42 A CLR $EF42
00200 00020A 5019 7F EF50 A CLR $EF50
00210 00021A 501C B6 9C A LDAA $B6C
00220 00022A 501E B7 EF52 A STAA $EF52
00230 00023A 5021 B6 04 A LDAA $4
00240 00024A 5023 B7 EF53 A STAA $EF53
00250 00025A 5026 B7 EF43 A STAA $EF43
00260 00026A 5029 7F EF52 A CLR $EF52 STOP HARDWARE SYSTEM
00270 00027A 502C B6 06 A LDAA $B6
00280 00028A 502E B7 EF41 A STAA $EF41
00290 00029A 5031 B7 EF51 A STAA $EF51
00300 00030A 5034 B6 EF50 A LDAA $EF50 CLR INTERRUPT
00310 00031A 5037 B6 EF52 A LDAA $EF52 INITIALIZE EVENT COUNTER
00320 00032A 503A B4 20 A ANDA $20
00330 00033A 503C 27 0A 5043 BEQ OUTLOP BUFFER EMPTY?
00340 00034A 503E 06 10 A LDAA $10 RAISE READ ENABLE
00350 00035A 5040 B7 EF52 A STAA $EF52

```

00360	00036A	5043	7F	EF52	A	CLR	\$EF52	
00370	00037A	5046	20	EF	5037	BRA	FLAG	RETURN, INITIAL DONE?
00380	00038A	5048	7F	533A	A	OUTLOP CLR	STABLE	LINE STABILITY CHECK
00390	00039A	504E	7F	5339	A	CLR	STB1	# OF NO DOT PASSES
00400	00040A	504E	7F	EF71	A	CLR	\$EF71	INITIALIZE MOTOR PIA
00410	00041A	5051	86	FF	A	LDAA	\$FF	
00420	00042A	5053	B7	EF70	A	STAA	\$EF70	
00430	00043A	5054	86	06	A	LDAA	\$6	
00440	00044A	505B	B7	EF71	A	STAA	\$EF71	
00450	00045A	505B	BD	50A2	A	GO JSR	COLECT	GO GET DATA FROM VIDEO
00460	00046A	505E	BD	525A	A	JSR	DIST	GO CALC ALTITUDE
00470	00047A	5041	FE	53D6	A	LDX	DOT	
00480	00048A	5064	27	0A	5070	BEQ	STA1	IS DOT (NOT) THERE?
00490	00049A	5066	7F	5339	A	CLR	STB1	IF DOT, CLR # NO DOTS
00500	00050A	5069	8C	0001	A	FILTER CPX	#1	
00510	00051A	506C	27	ED	505B	BEQ	GO	SYSTEM ERROR, TRY AGAIN
00520	00052A	506E	20	14	5084	BRA	RUN	RUN SYSTEM WITH GOOD DOT
00530	00053A	5070	86	01	A	STA1 LDAA	#1	# OF CONSEQ. NO DOT PASS
00540	00054A	5072	B0	5339	A	SUBA	STB1	
00550	00055A	5075	27	05	507C	BEQ	SEND	NO DOT TWICE?
00560	00056A	5077	7C	5339	A	INC	STB1	ACK ONE NO DOT PASS
00570	00057A	507A	20	DF	505B	BRA	GO	
00580	00058A	507C	7F	5339	A	SEND CLR	STB1	CLR # OF NO DOT PASSES
00590	00059A	507F	BD	5179	A	JSR	HUNT	GO HUNT FOR MISSING DOT
00600	00060A	5082	20	D7	505B	BRA	GO	RETURN AND TRY AGAIN
00610	00061A	5081	EC	5000	A	RUN CPX	CONV	RASTER LINE STAB. TEST
00620	00062A	5087	27	0C	5095	BEQ	SET1	CONVERGENT?
00630	00063A	5089	86	01	A	LDAA	#1	PUT STABLE BIT HERE
00640	00064A	508B	B0	533A	A	SUBA	STABLE	
00650	00065A	508E	27	0D	509D	BEQ	DRIVE	IS DOT NOT CONV?
00660	00066A	5090	7C	533A	A	INC	STABLE	ACK NOT CONV PASS
00670	00067A	5093	20	C6	505B	BRA	GO	RETURN AND TRY AGAIN
00680	00068A	5095	7F	533A	A	SET1 CLR	STABLE	
00690	00069A	5098	BD	525A	A	JSR	DIST	CALC DIST FOR ALTIM
00700	00070A	509B	20	BE	505B	BRA	GO	RETURN AND PROCESS AGAIN
00710	00071A	509D	BD	5200	A	DRIVE JSR	MOVE	GO TO MIRROR ADJUST SR.
00720	00072A	50A0	20	B9	505B	BRA	GO	RETURN AND REPROCESS
00730	00073A	50A2	7F	5359	A	COLECT CLR	LDATA	INITIALIZE DATA REG'S
00740	00074A	50A5	7F	535A	A	CLR	LDATA+1	
00750	00075A	50A8	7F	5395	A	CLR	DDATA	
00760	00076A	50AB	7F	5396	A	CLR	DDATA+1	
00770	00077A	50AE	7F	53D1	A	CLR	COUNT1	
00780	00078A	50B1	7F	53D2	A	CLR	NUMB1	
00790	00079A	50B4	7F	53D5	A	CLR	COUNT2	
00800	00080A	50B7	B6	EF50	A	LDAA	\$EF50	CLR H-WARE INTERRUPT
00810	00081A	50BA	86	80	A	LDAA	\$80	
00820	00082A	50BC	B7	EF52	A	STAA	\$EF52	START HARDWARE RUNNING
00830	00083A	50BF	86	FF	A	LDAA	\$FF	LOOP TIMER
00840	00084A	50C1	F6	EF51	A	JMP2 LDAB	\$EF51	CHECK FOR DOT INTERRUPT
00850	00085A	50C4	20	39	50FF	BMI	READ	IF SEE DOT, READ DATA
00860	00086A	50C6	FF	53D3	A	STX	DUMMY	PAD LOOP TIME
00870	00087A	50C9	FF	53D3	A	STX	DUMMY	
00880	00088A	50CC	FF	53D3	A	STX	DUMMY	
00890	00089A	50CF	FF	53D3	A	STX	DUMMY	
00900	00090A	50D2	FF	53D3	A	STX	DUMMY	
00910	00091A	50D5	FF	53D3	A	STX	DUMMY	
00920	00092A	50D8	FF	53D3	A	STX	DUMMY	
00930	00093A	50DB	FF	53D3	A	STX	DUMMY	
00940	00094A	50DE	FF	53D3	A	STX	DUMMY	
00950	00095A	50E1	FF	53D3	A	STX	DUMMY	
00960	00096A	50E4	FF	53D3	A	STX	DUMMY	
00970	00097A	50E7	FF	53D3	A	STX	DUMMY	
00980	00098A	50EA	FF	53D3	A	STX	DUMMY	
00990	00099A	50ED	FF	53D3	A	STX	DUMMY	
01000	00100A	50F0	7C	53D1	A	INC	COUNT1	# OF NO DOT LOOPS
01010	00101A	50F3	B1	53D1	A	CMPLA	COUNT1	\$FF LOOPS?
01020	00102A	50F6	26	C9	50C1	BNE	JMP2	RETURN AND TRY AGAIN
01030	00103A	50F8	CE	0000	A	LDX	#0	
01040	00104A	50FB	FF	53D3	A	STX	DOT	NO DOT FOUND
01050	00105A	50FE	39			RTS		RETURN TO MAIN PROG
01060	00106A	50FF	7F	EF52	A	READ CLR	\$EF52	STOP HARDWARE SYSTEM
01070	00107A	5102	B6	EF52	A	CHECK LDAA	\$EF52	
01080	00108A	5105	84	20	A	ANDA	\$120	CHECK BUFFER NOT EMPTY
01090	00109A	5107	27	3A	5143	BEQ	DCENTR	ALL DATA IN, GET CNTR
01100	00110A	5109	86	10	A	LDAA	\$110	ENABLE READ ENABLE
01110	00111A	510B	B7	EF52	A	STAA	\$EF52	
01120	00112A	510E	B6	EF40	A	LDAA	\$EF40	GET WIDTH AND UNPACK
01130	00113A	5111	16			TAB		SAVE FOR FUTURE UNPACKING
01140	00114A	5112	84	F0	A	ANDA	\$1F0	MASK OTHER INFO
01150	00115A	5114	44			LSRA		

01160	00116A	5115	44		LSRA		
01170	00117A	5116	44		LSRA		
01180	00118A	5117	81	03	CMFA	#3	MINIMUM WIDTH
01190	00119A	5119	2F	23	BLE	DISAB	IF TOO SMALL, SKIP
01200	00120A	511B	7D	53D5	TST	COUNT2	FIRSTGOODWIDTH?
01210	00121A	511E	26	1B	BNE	JMP4	IF NOT, GO
01220	00122A	5120	B6	EF42	LDAA	#EF42	FIRST GOOD LINE
01230	00123A	5123	43		COMA		
01240	00124A	5124	B7	535A	STAA	LDATA+1	STORE LSB OF RASTER LINE
01250	00125A	5127	17		TBA		
01260	00126A	5128	43		COMA		
01270	00127A	5129	84	01	ANDA	#1	
01280	00128A	512B	B7	5359	STAA	LDATA	STORE MSB OF RASTER LINE
01290	00129A	512E	D6	EF50	LDAA	#EF50	GET DISPLACEMENT DATA
01300	00130A	5131	B7	5396	STAA	DDATA+1	STORE LSB OF DISPLACEMENT
01310	00131A	5134	17		TBA		
01320	00132A	5135	84	0E	ANDA	#0E	
01330	00133A	5137	44		LSRA		
01340	00134A	5138	B7	5395	STAA	DDATA	
01350	00135A	513B	7C	53D5	JMP4	COUNT2	COUNT # OF GOOD DOTS
01360	00136A	513E	7F	EF52	DISAB	CLR	DISABLE READ ENABLE
01370	00137A	5141	20	BF	5102	BRA	CHECK
01380	00138A	5143	B6	53D5	DCENTR	LDAA	# OF LINES WITH A DOT
01390	00139A	5146	B7	53DC	A	STAA	WDCNT
01400	00140A	5149	FE	5359	A	LDX	LINE
01410	00141A	514C	FF	53D8	A	STX	LINE
01420	00142A	514F	FE	5395	A	LDX	DDATA
01430	00143A	5152	FF	53DA	A	STX	MAX
01440	00144A	5155	74	53DC	A	LSR	WDCNT
01450	00145A	5158	B6	53D9	A	LDAA	LINE+1
01460	00146A	515B	BB	53DC	A	ADDA	WDCNT
01470	00147A	515E	B7	53D7	A	STAA	DOT+1
01480	00148A	5161	B6	53D8	A	LDAA	LINE
01490	00149A	5164	B7	00	A	ADCA	#0
01500	00150A	5166	B7	53D6	A	STAA	DOT
01510	00151A	5169	B6	53D7	A	LDAA	DOT+1
01520	00152A	516C	84	01	A	ANDA	#1
01530	00153A	516E	27	01	5171	BEQ	ADD1
01540	00154A	5170	39		RTS		
01550	00155A	5171	FE	53D6	A	LDX	DOT
01560	00156A	5174	08		INX		
01570	00157A	5175	FF	53D6	A	STX	DOT
01580	00158A	5178	39		RTS		
01590	00159A	5179	CE	00FF	A	LDX	#0FF
01600	00160A	517C	FF	53DF	A	STX	INFIN
01610	00161A	517F	CE	FF54	A	LDX	#FF54
01620	00162A	5182	FF	53DD	A	STX	ZERO
01630	00163A	5185	ED	50A2	A	JSR	COLECT
01640	00164A	5188	FE	53D6	A	LDX	DOT
01650	00165A	518B	26	72	51FF	BNE	JUMP
01660	00166A	518D	B6	EF08	A	LDAA	#EF08
01670	00167A	5190	01		NOP		
01680	00168A	5191	FE	EF08	A	LDX	#EF08
01690	00169A	5194	FF	53E1	A	STX	LOCA
01700	00170A	5197	B6	53E2	A	LDAA	LOCA+1
01710	00171A	519A	B0	53DE	A	SUBA	ZERO(1)
01720	00172A	519D	B7	53E4	A	STAA	DIFF+1
01730	00173A	51A0	B6	53E1	A	LDAA	LOCA
01740	00174A	51A3	B2	53DD	A	SECA	ZERO
01750	00175A	51A6	B7	53E3	A	STAA	DIFF
01760	00176A	51A9	FE	53E3	A	LDX	DIFF
01770	00177A	51AC	2F	11	51EF	BLE	MINFIN
01780	00178A	51AE	7F	EF70	A	CLR	#EF70
01790	00179A	51B1	01		NOP		
01800	00180A	51B2	01		NOP		
01810	00181A	51B3	01		NOP		
01820	00182A	51B4	01		NOP		
01830	00183A	51B5	01		NOP		
01840	00184A	51B6	01		NOP		
01850	00185A	51B7	01		NOP		
01860	00186A	51B8	B6	08	A	LDAA	#08
01870	00187A	51BA	B7	EF70	A	STAA	#EF70
01880	00188A	51BD	20	C6	51B5	BRA	MZERO
01890	00189A	51BF	ED	50A2	A	JSR	COLECT
01900	00190A	51C2	FE	53D6	A	LDX	DOT
01910	00191A	51C5	26	38	51FF	BNE	JUMP
01920	00192A	51C7	B6	EF08	A	LDAA	#EF08
01930	00193A	51CA	01		NOP		
01940	00194A	51CB	FF	EF08	A	LDX	#EF08

01950	00195A	51CE	FF	53E1	A	STX	LOCA	STORE MIRROR LOCATION
01960	00196A	51D1	B6	53E2	A	LDAA	LOCA+1	D. P. SUBTR FOR DONE TEST
01970	00197A	51D4	B0	53E0	A	SUBA	INFIN+1	LSB SUBTRACT
01980	00198A	51D7	B7	53E4	A	STAA	DIFF+1	STORE LSB RESULT
01990	00199A	51DA	B6	53E1	A	LDAA	LOCA	
02000	00200A	51DD	B2	53DF	A	SBCA	INFIN	MSB SUBTRACT
02010	00201A	51E0	B7	53E3	A	STAA	DIFF	STORE MSB RESULT
02020	00202A	51E3	FE	53E3	A	LDX	DIFF	CHECK IF DONE
02030	00203A	51E6	2C	11 51F9		BGE	DIE	IF NO DOT, DIE
02040	00204A	51E8	7F	EF70	A	CLR	\$EF70	MOVE MIRROR TO INFINITY
02050	00205A	51EB	01			NOP		
02060	00206A	51EC	01			NOP		
02070	00207A	51ED	01			NOP		
02080	00208A	51EE	01			NOP		
02090	00209A	51EF	01			NOP		
02100	00210A	51F0	01			NOP		
02110	00211A	51F1	01			NOP		
02120	00212A	51F2	B6	AB	A	LDAA	#\$AB	
02130	00213A	51F4	B7	EF70	A	STAA	\$EF70	MOVE MIRROR
02140	00214A	51F7	20	C6 51EF		BRA	MINFIN	RETURN AND LOOK FOR DOT
02150	00215A	51F9	B6	3F	A DIE	LDAA	#\$3F	
02160	00216A	51FB	B7	51FE	A	STAA	BK	
02170	00217A	51FE	01		BK	NOP		
02180	00218A	51FF	39			JUMP	RTS	
02190	00219							
02200	00220							
02210	00221							
02220	00222A	5200	B6	5001	A	MOVE	LDAA	CONV+1
02230	00223A	5203	B0	53D7	A		SUBA	DOT+1
02240	00224A	5206	B7	53F4	A		STAA	LOC+1
02250	00225A	5209	B6	5000	A		LDAA	CONV
02260	00226A	520C	B2	53D6	A		SBCA	DOT
02270	00227A	520F	B7	53F3	A		STAA	LOC
02280	00228A	5212	7F	53F5	A		CLR	MM
02290	00229A	5215	FE	53F3	A		LDX	LOC
02300	00230A	5218	27	3F 5259			GOBACK	NO MOVE IF CONVERGENT
02310	00231A	521A	8C	01A0	A		CPX	#\$1A0
02320	00232A	521D	27	3A 5259			GOBACK	SYSTEM ERROR FILTER
02330	00233A	521F	FE	53F3	A		LDX	LOC
02340	00234A	5222	2B	1B 520F			BMI	MOVUP
02350	00235A	5224	B6	20	A	MOVDN	LDAA	#\$20
02360	00236A	5226	B7	53F5	A		STAA	MM
02370	00237A	5229	BD	53FE	A		JSR	CLCMV
02380	00238A	522C	7F	EF70	A		CLR	\$EF70
02390	00239A	522F	01				NOP	
02400	00240A	5230	01				NOP	
02410	00241A	5231	01				NOP	
02420	00242A	5232	01				NOP	
02430	00243A	5233	01				NOP	
02440	00244A	5234	01				NOP	
02450	00245A	5235	01				NOP	
02460	00246A	5236	B6	53F5	A		LDAA	MM
02470	00247A	5239	B7	EF70	A		STAA	\$EF70
02480	00248A	523C	7E	5259	A		JMP	GOBACK
02490	00249A	523F	B6	53F4	A	MOVUP	LDAA	LOC+1
02500	00250A	5242	40				NEGA	
02510	00251A	5243	B7	53F4	A		STAA	LOC+1
02520	00252A	5246	BD	53FE	A		JSR	CLCMV
02530	00253A	5249	7F	EF70	A		CLR	\$EF70
02540	00254A	524C	01				NOP	
02550	00255A	524D	01				NOP	
02560	00256A	524E	01				NOP	
02570	00257A	524F	01				NOP	
02580	00258A	5250	01				NOP	
02590	00259A	5251	01				NOP	
02600	00260A	5252	01				NOP	
02610	00261A	5253	B6	53F5	A		LDAA	MM
02620	00262A	5256	B7	EF70	A		STAA	\$EF70
02630	00263A	5259	39			GOBACK	RTS	RETURN TO MAIN PROG
02640	00264A	525A	B6	EF08	A	DIIST	LDAA	\$EF08
02650	00265A	525D	01				NOP	
02660	00266A	525F	FE	EF08	A		LDX	\$EF08
02670	00267A	5261	FF	53EF	A		STX	MIRAD
02680	00268A	5264	B6	53F0	A		LDAA	MIRAD+1
02690	00269A	5267	8B	FF	A		ADDA	#\$FF
02700	00270A	5269	B7	53F2	A		STAA	TOFSET+1
02710	00271A	526C	B6	53EF	A		LDAA	MIRAD
02720	00272A	526F	89	03	A		ADCA	#3
02730	00273A	5271	B7	53F1	A		STAA	TOFSET
								STORE MSB IN TABLE OFFSET

02740	00274A	5274	B6	53F2	A	LDAA	TOFSET+1	MULTIPLY BY 1.5 TO APPROX SCALE OUTPUT**
02750	00275A	5277	B8	53F2	A	ADDA	TOFSET+1	FOR D. P. DATA
02760	00276A	527A	B7	53F2	A	STAA	TOFSET+1	STORE LSB
02770	00277A	527D	B6	53F1	A	LDAA	TOFSET	
02780	00278A	5280	B9	53F1	A	ADCA	TOFSET	ADD MSB
02790	00279A	5283	B7	53F1	A	STAA	TOFSET	STORE MSB
02800	00280A	5286	B6	53F1	A	LDAA	TOFSET	ADD IN TABLE INITIALIZE
02810	00281A	5289	B8	75	A	ADDA	#475	LOCATE TABLE AT \$7000
02820	00282A	528D	B7	53F1	A	STAA	TOFSET	STORE IN MSB
02830	00283A	528E	FE	53F1	A	LDX	TOFSET	GET TABLE OFFSET
02840	00284A	5291	FF	5295	A	STX	FLAG+1	INJECT IN DATA RETR. LOCA
02850	00285A	5294	FE	7000	A-FLAG1	LDX	\$7000	GET OUTPUT DATA FROM TABLE
02860	00286A	5297	FF	53F6	A	STX	TEMP2	STORE TO DO BIAS & SCALE
02870	00287A	529A	FF	53F9	A	STX	ER1	STORE FOR ERROR CALC
02880	00288A	529D	B6	53F7	A	LDAA	TEMP2+1	ADD LSB BIAS FACTOR
02890	00289A	52A0	B8	5006	A	ADDA	BIAS+1	LSB ADD
02900	00290A	52A3	B7	53F7	A	STAA	TEMP2+1	STORE BIASED LSB
02910	00291A	52A6	B6	53F6	A	LDAA	TEMP2	
02920	00292A	52A9	B9	5005	A	ADCA	BIAS	ADD MSB BIAS FACTOR
02930	00293A	52AC	B7	53F6	A	STAA	TEMP2	STORE BIASED MSB
02940	00294							
02950	00295A	52AF	B6	53F6	A	LDAA	TEMP2	GET MSB OF VOLTAGE
02960	00296A	52B2	44			LSRA		DIVIDE BY 2
02970	00297A	52B3	B7	53F8	A	STAA	TEMP3	STORE MSB QUOTIENT
02980	00298A	52B6	B6	53F7	A	LDAA	TEMP2+1	GET LSB OF VOLTAGE
02990	00299A	52B9	44			RORA		DIVIDE BY 2 (PULL CARRY IN)
03000	00300A	52BA	B7	53F9	A	STAA	TEMP3+1	STORE LSB QUOTIENT
03010	00301A	52BD	B6	53F7	A	LDAA	TEMP2+1	ADD FOR 1.5 SCALE FACTOR
03020	00302A	52C0	B8	53F9	A	ADDA	TEMP3+1	LSB ADD
03030	00303A	52C3	B7	53F8	A	STAA	INSOUT+1	STORE LSB OF ALTIM OUTPUT
03040	00304A	52C6	B6	53F8	A	LDAA	TEMP3	
03050	00305A	52C9	B9	53F6	A	ADCA	TEMP2	MSB ADD
03060	00306A	52CC	B7	53FA	A	STAA	INSOUT	STORE MSB OF ALTIM OUTPUT
03070	00307A	52CF	FE	53FA	A	LDX	INSOUT	GET BIASED AND SCALED VALUE
03080	00308A	52D2	FF	EF20	A	STX	\$EF20	DO D/A CONV FOR ALTIM OUTPUT
03090	00309A	52D5	FE	53E9	A	LDX	ER1	GET ORIG TABLE VALUE
03100	00310A	52D8	FF	EF24	A	STX	\$EF24	DO D/A FOR STRIP CHART
03110	00311A	52DB	B6	EF0C	A	LDAA	\$EF0C	
03120	00312A	52DE	01			NOP		
03130	00313A	52DF	FE	EF0C	A	LDX	\$EF0C	GET TRACK VOLTAGE
03140	00314A	52E2	FF	53EB	A	STX	ER2	STORE FOR ERROR CALC
03150	00315A	52E5	B6	53FA	A	LDAA	ER1+1	D. P. SUBTR FOR ERROR CALC
03160	00316A	52E8	B0	53EC	A	SUBA	ER2+1	LSB SUBTR
03170	00317A	52EB	B7	53LE	A	STAA	ERROR+1	LSB ERROR
03180	00318A	52EE	B6	53L9	A	LDAA	ER1	
03190	00319A	52F1	B2	53LE	A	SBCA	ER2	MSB SUBTRACT
03200	00320A	52F4	B7	53ED	A	STAA	ERROR	MSB ERROR
03210	00321A	52F7	FE	53ED	A	LDX	ERROR	GET FINAL ERROR VALUE
03220	00322A	52FA	FF	EF22	A	STX	\$EF22	DO D/A FOR STRIP CHART
03230	00323A	52FD	39			RTS		
03240	00324A	52FE	B6	53F4	A	LDAA	LOC+1	
03250	00325A	5301	B1	5002	A	CMFA	SHNV	MAKE A SMALL MOV'T?
03260	00326A	5304	2D	27	532D	BLT	SMALL	
03270	00327A	5306	B1	5003	A	CMFA	MDMV	MAKE A MEDIUM MOV'T?
03280	00328A	5309	2D	10	5323	BLT	MED	
03290	00329A	530B	B1	5004	A	CMFA	LGMV	MAKE A LARGE MOV'T?
03300	00330A	530E	2D	0A	531A	BLT	LARGE	
03310	00331A	5310	B6	84	A	LDAA	#84	LARGEST POSS MOV'T
03320	00332A	5312	F6	53F5	A	LDAB	MM	GET DIRECTION
03330	00333A	5315	1B			ABA		COMBINE
03340	00334A	5316	B7	53F5	A	STAA	MM	STORE COMPLETED MOV'T
03350	00335A	5319	39			RTS		
03360	00336A	531A	B6	83	A	LDAA	#83	LARGE MOV'T
03370	00337A	531C	F6	53F5	A	LDAB	MM	GET DIRECTION
03380	00338A	531F	1B			ABA		COMBINE
03390	00339A	5320	B7	53F5	A	STAA	MM	STORE COMPLETED MM
03400	00340A	5323	B6	82	A	LDAA	#82	MEDIUM MOV'T
03410	00341A	5325	F6	53F5	A	LDAB	MM	GET DIRECTION
03420	00342A	5328	1B			ABA		COMBINE
03430	00343A	5329	B7	53F5	A	STAA	MM	STORE MOTOR MOV'T
03440	00344A	532C	39			RTS		
03450	00345A	532D	B6	81	A	LDAA	#81	SMALLEST POSS MOV'T
03460	00346A	532F	F6	53F5	A	LDAB	MM	GET DIRECTION
03470	00347A	5332	1B			ABA		COMBINE
03480	00348A	5333	B7	53F5	A	STAA	MM	STORE MOV'T
03490	00349A	5336	39			RTS		
03500	00350A	5337	0002	A	VARI	RMB	2	
03510	00351A	5339	0001	A	STBL	RMB	1	# OF NO DOT PASSES
03520	00352A	533A	0001	A	STABLE	RMB	1	# OF LINE STABLE PASSES

03530	00353A	533B	001E	A WDATA	RMB	30	WIDTH OF DOT DATA
03540	00354A	5359	003C	A LDATA	RMB	60	RASTER LINE # DATA
03550	00355A	5395	003C	A DDATA	RMB	60	DISPLACEMENT DATA
03560	00356A	53D1	0001	A COUNT1	RMB	1	# OF COLLECT PASSES
03570	00357A	53D2	0001	A NUMB1	RMB	1	
03580	00358A	53D3	0002	A DUMMY	RMB	2	DUMMY TIME PAD VAR.
03590	00359A	53D5	0001	A COUNT2	RMB	1	# OF LINES WITH A GOOD DOT
03600	00360A	53D4	0002	A DOT	RMB	2	LOCATION OF DOT CENTER
03610	00361A	53D8	0002	A LINE	RMB	2	TEMP STORE FOR DOT CENTER
03620	00362A	53DA	0002	A MAX	RMB	2	SAME AS ABOVE
03630	00363A	53DC	0001	A WDCNT	RMB	1	# OF LINES W/ A GOOD DOT
03640	00364A	53DD	0002	A ZERO	RMB	2	MIRROR VOLTAGE @ DIST=0
03650	00365A	53DF	0002	A INFIN	RMB	2	MIRROR VOLTAGE @ D=INFIN
03660	00366A	53E1	0002	A LOCA	RMB	2	CURRENT VOLTAGE OF MIRROR
03670	00367A	53E3	0002	A DIFF	RMB	2	DIFF BETW LOCA AND GOAL
03680	00368A	53E5	0002	A TEMP1	RMB	2	TEMP REG FOR MOV'T CALC
03690	00369A	53E7	0002	A TADD	RMB	2	TABLE ADDRESS
03700	00370A	53E9	0002	A ER1	RMB	2	SYSTEM ERROR VAR 1
03710	00371A	53EB	0002	A ER2	RMB	2	SYSTEM ERROR VAR 2
03720	00372A	53ED	0002	A ERROR	RMB	2	RESULTANT SYSTEM ERROR
03730	00373A	53EF	0002	A MIRAD	RMB	2	MIRROR VOLTAGE FOR DIST
03740	00374A	53F1	0002	A TOSSET	RMB	2	TABLE OFFSET (BIAS)
03750	00375A	53F3	0002	A LOC	RMB	2	# OF LINES OFF CONVERGE
03760	00376A	53F5	0001	A MM	RMB	1	MOTOR MOVEMENT
03770	00377A	53F6	0002	A TEMP2	RMB	2	TEMP REG FOR DIST CALC
03780	00378A	53F8	0002	A TEMP3	RMB	2	TEMP REG FOR DIST CALC
03790	00379A	53FA	0002	A INSOUT	RMB	2	ALTIMETER OUTPUT VOLTAGE
03800	00380A	53FC	39	RETU	RTS		
03810	00381				END		
TOTAL ERRORS 00000--00000							

5171 ADD1 00153 00155\*  
5005 BIAS 00013\*00289 00292

51FE EK 00216 00217\*  
5102 CHECK 00107\*00137  
52FE CLCMV 00237 00252 00324\*  
50A2 COLECT 00045 00073\*00143 00189  
5000 CONV 00009\*00061 00222 00225  
53D1 COUNT1 00077 00100 00101 00356\*  
53D5 COUNT2 00079 00120 00135 00138 00359\*  
5143 DCENTR 00109 00138\*  
5395 DDATA 00075 00076 00130 00134 00142 00355\*  
51F9 DIE 00203 00215\*  
53E3 DIFF 00172 00175 00176 00198 00201 00202 00367\*  
513E DISAB 00119 00136\*  
525A DIST 00046 00069 00264\*  
53D6 DOT 00047 00104 00147 00150 00151 00155 00157 00164 00190 00223 00226 00360\*  
509D DRIVE 00065 00071\*  
53D3 DUMMY 00086 00087 00088 00089 00090 00091 00092 00093 00094 00095 00096 00097  
00098 00099 00353\*  
53E9 ER1 00287 00309 00315 00318 00370\*  
53EB ER2 00314 00316 00319 00371\*  
53ED ERROR 00317 00320 00321 00372\*  
5069 FILTER 00050\*  
5037 FLAG 00031\*00037  
5294 FLAG1 00284 00285\*  
505B GO 00045\*00051 00057 00060 00067 00070 00072  
5259 GOECK 00230 00232 00248 00263\*  
5179 HUNT 00059 00159\*  
53DF INFIN 00160 00197 00200 00365\*  
53FA INSOUT 00303 00306 00307 00379\*  
50C1 JMP2 00084\*00102  
513B JMP4 00121 00135\*  
51FF JUMP 00165 00191 00218\*  
531A LARGE 00330 00336\*  
5359 LDATA 00073 00074 00124 00128 00140 00354\*  
5004 LGMV 00012\*00329  
5310 LCST 00331\*  
53D8 LINE 00141 00145 00148 00361\*  
53F3 LOC 00224 00227 00229 00233 00249 00251 00324 00375\*  
53E1 LOCA 00169 00170 00173 00195 00196 00199 00366\*  
5124 MARK2 00124\*  
5131 MARK3 00130\*  
53DA MAX 00143 00362\*  
5003 MDMV 00011\*00327  
5323 MED 00328 00346\*

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51BF MINFIN 00177 00189*00214
53EF MIRAD 00267 00268 00271 00373*
53F5 MM 00228 00236 00246 00261 00332 00334 00337 00339 00341 00343 00346 00348
00376*
5200 MOVE 00071 00222*
5224 MVDN 00235*
523F MVUP 00234 00249*
5185 MZERO 00163*00188
53D2 NUMB1 00078 00357*
5048 OUTLOP 00033 00038*
50FF READ 00085 00106*
53FC RETU 00380*
5084 RUN 00052 00061*
507C SEND 00055 00058*
5095 SET1 00062 00068*
532D SMALL 00326 00345*
5002 SMMV 00010*00325
5070 STA1 00048 00053*
533A STABLE 00038 00064 00066 00068 00352*
5339 STB1 00039 00049 00054 00056 00058 00351*
53E7 TADD 00369*
53E5 TEMP1 00368*
53F6 TEMP2 00286 00288 00290 00291 00293 00295 00298 00301 00305 00377*
53F8 TEMP3 00297 00300 00302 00304 00378*
53F1 TDFSET 00270 00273 00274 00275 00276 00277 00278 00279 00280 00282 00283 00374*
5337 VARI 00350*
533B WDATA 00353*
53DC WDCNT 00139 00144 00146 00363*
53DD ZERO 00162 00171 00174 00364*

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I claim:

1. In a method for determining the altitude of a flight simulator probe moving relative to and above the terrain of a flight simulator model wherein the imaginary line extending from the probe in a direction normal to the model is characterized as the probe plumb line, the steps of:

- directing a pencil-like beam of radiation from said probe onto the model keeping said beam within a plane containing said probe plumb line to produce a beam spot on said model;
- detecting the location of said beam spot relative to two orthogonal coordinates with a detector situated remote from said probe plumb line and having a linear sensitivity zone optically aligned with said probe plumb line;
- varying the angular orientation of the beam within said probe plumb line plane and relative to a reference plane so as to cause said beam spot to impinge on the model site intersected by said probe plumb line;
- determining the angular orientation of the beam relative to said reference plane; and
- utilizing the determined angular orientation of said beam to determine the altitude of said probe over the terrain of the model.

2. The method of claim 1 including the step of, directing a second beam of radiation onto the terrain of the model from a position on the probe angularly spaced from the position of the first beam taken about an axis of revolution generally coaxially of said probe plumb line; and detecting the second beam spot when said first beam spot is obstructed by the terrain from reaching the intersection of the model and the probe plumb line.

3. The method of claim 1 wherein said beam of radiation is a beam of monochromatic, collimated light.

4. The method of claim 1 wherein the step of detecting the beam spot includes the step of directing a beam spot image through a light pipe on a path between the beam spot and the detector.

5. The method of claim 2 wherein the step of directing the second beam of radiation onto the terrain includes the step of splitting off of the first beam a portion of its energy to produce said second beam.

6. In a flight simulator apparatus of the type where a probe simulates an aircraft and the simulator operator controls the motion of the probe relative to the terrain of a model while viewing said model via a video monitor on said probe:

means for directing a pencil-like beam of radiation from the probe onto the terrain of the model to produce a beam spot on the model where the beam impinges on the model, an imaginary line extending from said probe normal to said model being known as the probe plumb line;

means supported by said probe for detecting the location of said beam impingement on said model, said means being remote from said probe plumb line, being two-dimensionally sensitive, and having a linear sensitivity zone in optical alignment with said probe plumb line;

servo means coupled to said beam directing means and said detecting means for varying the angular direction of the beam in a plane containing the probe plumb line and maintaining the beam spot on the model at the site where the probe plumb line intersects the model;

means for determining the angular orientation of the beam relative to a reference plane; and

means for utilizing the determined angular orientation of said beam to determine the distance between said probe and said model measured along said probe plumb line.

7. The apparatus of claim 6 including:

means for directing a second beam of radiation onto the terrain of the model from a position on the probe angularly spaced from the position of the first beam taken about an axis of revolution generally coaxial of said probe plumb line; and means for detecting the second beam spot when said first beam spot is obstructed by the terrain from



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reaching the model site intersected by the probe plumb line.

8. The apparatus of claim 6 wherein said means for directing a pencil-like beam of radiation includes means for directing a pencil-like beam of monochromatic, collimated light.

9. The apparatus of claim 6 including light pipe means

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for directing an image of said beam spot to said detecting means.

10. The apparatus of claim 7 including beam splitter means for splitting off a portion of said first beam to produce said second beam.

11. The apparatus of claim 6 wherein said detecting means includes a video camera.

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